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ELEVATED TEMPERATURE PROPERTIES OF CAST ALUMINUM ALLOYS A201-T7 AND A357-T6

J. D. Tirpak, First Lieutenant, USAF Materials Integrity Branch Systems Support Division

November 1985

YECEMBEK
Final Report for Period 1982-December 1984



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JON D. TIRPAK, LT, USAF Engineering Design Data Materials Engineering Branch Systems Support Division CLAYTON L. HARMSWORTH, Tech Mgr Engineering Design Data Materials Engineering Branch Systems Support Division

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THEODORE J. REINHART, Chief Materials Engineering Branch Systems Support Division Materials Laboratory

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A201-T7 elongation increased	as temperature	Increased. T	ed markedly he tensile	strength of	The f
decreased as test temperature	increased. A3!	57-T6 ductili	ty increase	d then deci	reased as
temperature increased. Valid	I fracture tough.	iess values w	ere difficu	It to obtain	in for
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### PREFACE

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### SECTION I

### BACKGROUND

In the past, little emphasis has been placed on the durability and damage tolerance of cast aluminum alloys A201-T7 and A357-T6. However, several systems originated requests for such data demonstrate that not only are aluminum castings being used, but their use is also desired in critical applications where damage tolerance design data is required. Both the aerospace industry and the Air Force are aware of this data need which must be filled before aerospace structural castings can be used in fracture critical applications. Northrop Corporation, under Air Force contract, developed much of the technology and data base to get cast aluminum data into MIL-HBK-5. 1-2 A part of this effort involved obtaining castings from several sources and developing an aluminum castings data base.

As part of this program, the Systems Support Division (AFWAL/MLSE) conducted fatigue crack growth testing. In addition, and in order to generate the data requested by the System Program Offices, elevated temperature tests were added to the program. These tests included tensile, plane strain fracture toughness, constant-load-amplitude fatigue crack growth, and constant-load-amplitude-fatigue.

This report contains the the data generated for A201-T7 and A357-T6 at 250°F and 400°F.

### SECTION II

### TEST PROGRAM AND PROCEDURES

A. The materials evaluated in this program were the aluminum casting alloys A201-T7 and A357-T6. A201 is an aluminum-copper-silver alloy and A357 is an aluminum-silicon-magnesium alloy (Table I). Both alloys have respectable properties and are commonly used in aerospace applications. For this program test plates were cast and heat treated to Mil-A-21180 requirements (Figure 1 and Table II).

The A201 plates were x-ray Grade "B" in the designated areas and x-ray Grade "C" in the non-designated areas. Surface penetrant inspection revealed no linear surface defects, and attached tensile coupons confirmed the heat treatment with tensile values of 60 ksi ultimate tensile strength (UTS) and 55 ksi yield tensile strength (YTS). Also, the minimum plate hardness was Rockwell B 70, and the minimum plate conductivity was 31% IAC.

The A357 plates were also x-ray Grade "B" and "C" in the designated and non-designated areas, respectively. The plate had no linear defects and met the specified tensile requirements.

B. Test specimens were excised from the designated areas of the castings and machined to the dimensions shown in Figures 2-4. The thicknesses (B), for both the fracture toughness and the fatigue crack growth specimens, were machined as thick as possible while maintaining the required surface finish.

TABLE I

Average Chemistries of Step Flates.

	A201-T7	A357-T6
Copper	4.7	0.01
Silicon	0.08	6.87
Tron	0.04	0.07
Manganese	0.3	0.01
Zinc		0.01
Magnesium	0.3	0.53
Titanium	0.24	0.17
Beryllium		0.029
Silver	0.45	
Aluminum	Balance	Balance

<sup>\*</sup> Slightly lower than MIL-21180C chemical composition limits.

igure 1: Step plate casting.

TABLE II
Heat Treatments

SUPPLIER	A201-T7	A357-T6
A	-Solutionize @ 940°F, 1 hr. @ 960°F, 1 hr. @ 980°F, 12 hrs.	
	-Water quench @ room temp. -Age @ 370°F, 5 hrs.	
В	-Solutionize @ 920°F, 2 hrs. @ 940°F, 2 hrs. @ 960°F, 2 hrs. @ 980°F, 18 hrsWater quench @ room tempAge @ 310°F, 5 hrs.	
C	## <b>#</b>	-Solutionize @ 1010°f, 12 hrsWater quench @ romma tempAge @ 330°F, 5 hrs.
D	*****	-Solutionize @ 1010°F, 16 hrsWater quench @ room tempAge @ 340°F, 6 hrs.

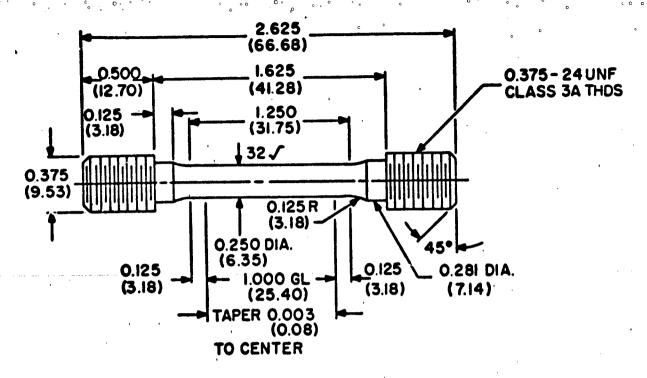


Figure 2: Tensile test specimen.

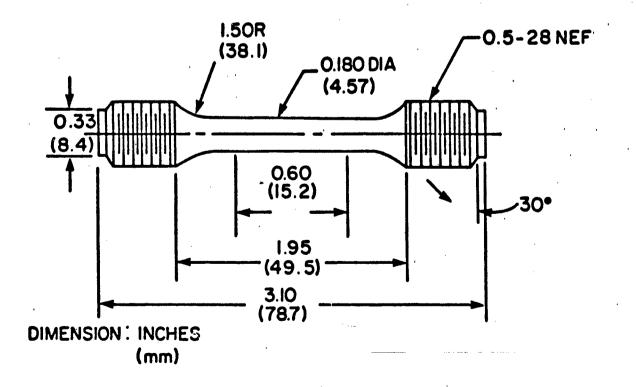
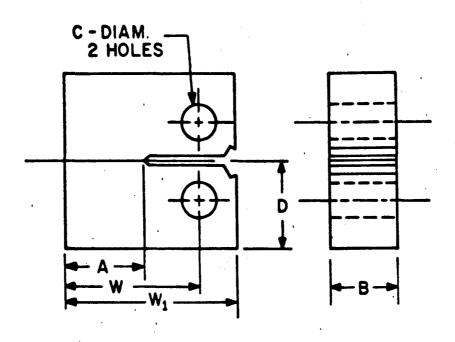


Figure 3: Fatigue test specimen.



Fracture Toughness

Fatigue Crack Growth

В	Α	Ŵ	Wl	D	C
<b>0.</b> 500 <b>(12.7)</b>	0.625 (15.9)	1.000 (25.4)	1.250 (31.8)	0.600	<b>0</b> .25 (6.4)
0.50 (12.7)	1.50 (38.1)	2.000 (50.8)	2.500 (63.5)	1.200 (30.5)	0.50 (12.7)

# DIMENSIONS IN INCHES (mm)

Figure 4: Fracture toughness and fatigue crack growth specimens.

C. The test procedures are briefly described as follows:

Tensile tests were conducted in accordance with ASTM Test Methods B 557 and E 21. Tests were performed on a 10 kip Instron tensile test machine with a Conrad-Missimer environmental chamber.

Plane strain fracture toughness test specimens were precracked on a 2.2 kip MTS axial electrohydraulic fatigue machine and then pulled on 10 kip tensile test machine with the specimen in a Conrad-Missimer ervironmental chamber. Tests were governed by ASTM Test Method E 399.

Fatigue crack growth specimens were tested as outlined in ASTM Test
Method E 647. Tests were conducted on an MTS axial ratigue machine
and Conred-Missimer convection heating chamber.

Constant-load-amplitude fatigue tests were conducted as outlined in ASTM Test Method F 466. Tests were conducted on a 2.. kip MTS axial tatigue machine with a split furnace surrounding the spe imer and grips.

All tests were conducted in air while test temperatures were kept within  $\pm$  2.5° F.

### SECTION 111

#### RESULTS AND DISCUSSION

A. Tensile test results for A201-T7 were listed in Tables III and IV. A201-T7 room temperature tensile properties for the step plate castings were 65.1 ksi UTS,60.0 ksi YTS, and 4.8% elongation. 4 At 250°F, A201-T7 averaged 59.1 ksi UTS, 54.6 ksi YTS and 9.3% elongation. At 400°F the A201-T7 tensile properties were 47.2 ksi UTS, 44.2 ksi YTS, and 11.8% elongation. Tensile test results for A357-T6 were listed in Tables V and VI. Room temperature tensile properties for A357-T6 step plate castings were of 48.8 ksi UTS, 41.1 ksi YTS, and 5.6% elongation. At 250°F the average tensile strength decreased to 43.3 ksi, the average yield strength dropped slightly to 39.3 ksi, and the average elongation increased to 10.1%. At 400°F, the average ultimate strength nearly equaled the average yield strength at 35.8 and 35.3 kmi, respectively. Also the elongation dropped off from 10.1% at 250°F to 8.0% at 400°F. B. Fracture toughness test data were listed in Tables VII-X. Of the twenty tests conducted, only three produced valid  $K_{T_{c}}$  values. A201-T7 had a wider range of  $K_0$  values than A357-T6; however, three of the A201-T7 values were valid. The average K<sub>TC</sub> value for A201-T7 at 250°F was 22.3 ksi $\sqrt{\text{in}}$  while the average K $_{0}$  value for A201-T7 at 400°F was 25.0 ksi√In. At 250°F and 400°F, the average Ko values for A357-T6 were 22.5 and 18.1 ksi vin, respectively. It was noted that the same problems occurred in this test program as those which occurred in the CAST Program. K<sub>TC</sub> values were not obtained because of thickness, crack length, crack curvature, and/or Pmax/Porequirements.6

TABLF III Tensile Test Results for A201-T7 at 250°F

2LT1 2LT2 2LT3 2LT4 2LT5 2LT5		derengen der MPa	(0.2% offset) ksi MPa	ffset) MPa	Z Elongation (1 in Gage Section)	of Area
2LT1 2LT2 2LT3 2LT4 2LT5 2LT5	0	8 907	55.3	381.3	11.5	28.4
2L12 2LT3 2LT4 2LT5 2LT6	53.0	0.864	57.7	397.8	4.0	7.0
2114 2114 2115 2116	2.70	377.2	50.2	346.1	7.6	29.1
2LT5 2LT5 2LT6	4 05	0.017	55.1	379.9	11.9	25.9
2LT6	0.60	408.2	54.1	373.0	9.3	21.8
	59.8	412.3	55.2	380.6	9.1	21.6
Average	59.16	407.4	54.6	376.5	9.3	22.3
		:			4.000.000	×
Specimen	Ultimate Strength ksi	nate ngth MPa	Yleid Strength (0.2% offset) ksi MPa	leid Strengtn (0.2% offset) ksi MPa	% Elongation (1 in Gage Section)	Reduction of Area
						•
2HT1*	1 9	1 6	יי ל יי	310 3	12.4	36.5
2HT2	ή· 8.4 	331.0	2.64	299.9	12.9	35.3
2HT 3	40.	0.000	0 K	315.8	10.0	29.5
2HT4	2.7	339.9	, C.	7.750	11.3	33.1
2HT5	, C4,	322.7	43.8	302.0	12.3	37.8
Zh16	0	, , ,				
Average	47.2	325.3	44.2	304.5	11.8	34.4

\* Failed in set up.

TABLE V Tensile Test Results for A357-T6 at 250°F

)+4	MPa 298.6 298.6 298.6 295.8	ks1	ks1 MPa		
43.3 43.3 42.9	298.6 298.6 298.6 295.8		<b>!</b>	(1 in Gage Section)	of Area
43.3 43.3	298.6 298.6 295.8 295.8	39.1	269.6	9.7	17.4
43.3	298.6 295.8 295.8	39.1	269.6	10.9	18.2
•	295.8 295.8	39.3	271.0	10.8	16.8
	295.8	#	*	7.2	11.6
47.3		39.3	271.0	12.5	18.8
43.5	299.9	39.6	273.0	9.3	16:3
43.3	298.6	39.3	271.0	10.1	. 16.5
Ulth	mate	Yield Strength	trength		×
 Strength	ngth	(0.2% c	(0.2% offset)	Z Elongation (1 in Gage Section)	Reduction of Area
164	8	104	3		
 .	1	ł	1	1	,
36.5	251.7	35.9	247.5	8.0	19.6
35.7	246.2	35.3	243.4	7.1	19.6
36.1	248.9	35.7	246.2	<b>8.</b>	21.8
35.3	243.4	34.8	239.9	8.6	23.8
35.3	243.4	34.6	238.6	8.3	22.4
35.8	246.8	35.3	246.8	0.8	21.4

TABLE VII Fracture Toughness Test Results for A201-T7 at 250°F

Specimen	Thickness (B,in)	Width (W, in)	Crack Length (a,in)	Pmax/PQ	Ksi /īn K	KIC MPa /m	Comments
2LK1	7967.0	1.0010	0.4844	1.04	23.4	25.7	Valid
2LK2	0.4955	0.9997	0.4924	1.04	20.8	22.9	Valid
2LK3	0.4959	0.9996	0.4937	1.0	22.8	25.1	Valid
2LK4	0.4973	0.9983	0.4950	1.0	27.3 1	30.0	Invalid 1,2,3
21.K5	0.4961	0.9982	0.4879	1.06	27.3 1	30.0	Invalid 1,2,3

1 K<sub>0</sub> 2 Exceeds thickness (B) requirement 3 Exceeds crack length (a) requirement

TABLE VIII Fracture Toughness Test Results for A201-T7 at 400°F

K<sub>Q</sub>=30 MPa√m

Ko=27.3 ksiJin, KIc=24.6 MPa./m

K<sub>Ic</sub>=22.3 ksi/in

Average

1.0 22.1 24.3 1.11 27.9 30.7 1.12 28.1 30.9	Invalid 1,2
27.9 28.1	Invalid 1.2.3
28.1	
700	Invalid 1,2,3
2.67	Invalid 1,2,3
27.0	Invalid 1,2,3
25.0 29.	
	25.0 29.5

l Violates thickness (B) requirement

2 Violates crack length (a) requirement

3 Pmax/P<sub>Q</sub> greater than 1.1

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TABLE IX Fracture Toughness Test Results for A357-T6 at 250°F

3LK1 3LK2 3LK3 3LK4 31K4	(B, in)	Width (W, 1n)	Crack Length (a,in)	Pmax/PQ	Kei /in "0	MPa /m	
3LK1 3LK2 3LK3 3LK4		, ,	2052 0	1.07	21.7	23.7	-
3LK2 3LK3 3LK4 31.K5	0.4783	000.1		70.	23.0	26.1	Inveltd 1,2,3
3LK3 3LK4 31 K5	0.4798	1.007	0.5409	) ·	71.6	22.5	_
3LK4	0.4796	1.007	0.5477	*O. I	0.12		
31.K5	0.4797	1,007	0.5392	1.07	22.3	24.3	-
	0 4795	1.006	0.5600	1.12	23.0	25.1	Invalld 1,2,3,4
		) ) ) •					
			•		22.5	24.5	
Average						,	٠
Specimen	Thickness (B,in)	Width (W, in)	Crack Length (a,in)	Pmax/PQ	Ksi /In Ko	MPa m	Comments
			9013.0	1 06	18.3	19.9	Invalid 1,2
3HK1	7025.0	1.004	0.515.0	-	17.6	19.2	Invalid 1.2
3HK2	0.4795	1.000	0.4989	11.1	2 6	6 61	
3HK3	0.4801	0.999	0.49/2	F. T • 1	70.7	10.0	
7XHL	0.4800	1.001	0.5428	1.09	0°/1	7.61	
3HK5	0.4798	0.999	0.5072	1.17	18.7	4.02	1
					18.1	19.7	

THE PROPERTY OF THE PROPERTY O

1 Violates thickness (B) requirement 2 Violates crack length (a) requirement C. Constant-load-amplitude fatigue data were listed in Tables XI-XIV and plotted in Figures 5-7. The A201-T7 curves were fairly smooth (Figures 5 and 7a) and were in good agreement with data generated in earlier investigations. There was a reduction in fatigue life for A201-T7 at both 250° and 400°F. The most significant reduction occurred at lives greater than 10<sup>5</sup> cycles. The fatigue endurance limit was approximately 14 ksi for A201-T7 at both temperatures.

The A357-T6 data exhibited more scatter than the A201-T7 data, but for the most part the A357-T6 fatigue curves were fairly smooth (Figures 6-7a). At 1x10<sup>6</sup> cycles there was little difference between the A357-T6 data at 250° and 400°F. The fatigue endurance limit was approximately 14 ksi. Although a room temperature data plot was constructed for A357-T6, these data can not be compared because of the different specimen configurations and R ratios. 8 In any event, A357-T6 has greater fatigue strength at 250° than at 400°F at below approximately  $4x10^5$  cycles. At lives greater than  $1x10^6$  cycles, the fatigue strength at both temperatures are nearly equal.

D. The constant-load-amplitude fatigue crack growth rate data were tabulated the Appendix and plotted in Figures 8-11. A201-T7 exhibited slightly faster growth at 400° than at 250°F at the lower stress intensity ranges. At the higher levels of stress intensity range, the crack growth rate data for both temperatures was nearly the same. Compared to other data, A201-T7 at 250° and 400°F had lower  $K_c$  values than room temperature data. During the testing of A201-T7, it was noticed that there was good agreement between the automated crack length measurements and the manual measurements at 250°F. This also occurred at 400°F for specimen 2HC2, but most attempts at 400°F to measure cracks

automatically failed so manual measurements were made instead.

The A357-T6 data also had faster crack growth rates at 400° than 250°F at the lower ranges of stress intensity. Both the 250° and 400°F fatigue crack growth rates were faster than at room temperature. 10

TABLE XI Fatigue Data for A201-T7 at 250°F, R=0.1

SPECIMEN	MAXIMUM STRESS (ks1)	CYCLES
2LF1	18	4.70×10 <sup>5</sup>
2LF2	40	4.03×10 <sup>4</sup>
2LF3	20	3.88×10 <sup>5</sup>
2LF4	••	
2LF5		
2LF6	30	9.30×10 <sup>4</sup>
2LF7	45	1.30×10 <sup>4</sup>
2LF8	52	1.20x10 <sup>4</sup>
2LF9	15	1.60×10 <sup>6</sup>
2LF10	25	2.60x10 <sup>5</sup>
2LF11	60	1.10×10
2LF12*	14	1.05×10 <sup>7</sup>
2LF13	35	6.50×10 <sup>4</sup>
2LF14	56	8.10×10 <sup>2</sup>

<sup>\*</sup>Runout

TABLE XII Fatigue Data for A201-T7 at 400°F, R=0.1

SPECIMEN	MAXIMUM STRESS (ksi)	CYCLES
2HF1	'25	1.23x10 <sup>5</sup>
2HF2	18	4.37×10 <sup>5</sup>
2HF3	50	8.30×10 <sup>3</sup>
2HF4	40	1.56x10 <sup>4</sup>
2HF5	58	2.70x10 <sup>3</sup>
2HF6	54	4.30x10 <sup>3</sup>
2HF7	20	1.72×10 <sup>5</sup>
2HF8	45	1.23x10 <sup>4</sup>
2HF9	35	5.02x10 <sup>4</sup>
2HF10	30	5.34x10 <sup>4</sup>
2HF11**	16	1.60x10 <sup>6</sup>
2HF12	<b></b> ·	معروضهم
2HF13*	15	1.00x10
2HF14	16	2.82x10

<sup>\*</sup>Runout

<sup>\*\*</sup>Failed in threads

TABLE XIII Fatigue Data for A357-T6 at 250°F, R=0.1

PECIMEN	MAXIMUM STRESS (ksi)	CYCLES
3LF1	50	2.00x10 <sup>2</sup>
3LF2	40	6.48×10 <sup>4</sup>
3LF3	30	4.63x10 <sup>5</sup>
3LF4	45	$6.70 \times 10^3$
3LF5	35	3.93x10 <sup>4</sup>
3LF6	25	4.34x10 <sup>5</sup>
3LF7	20	1.37×10 <sup>6</sup>
3LF8*	15	1.01x10 <sup>7</sup>
3LF9	17.5	9.44x10 <sup>5</sup>
3LF10	32	2.45×10 <sup>5</sup>
3LF11 ·	. 42	5.19x10 <sup>4</sup>
3LF12	34	1.38x10 <sup>5</sup>
3LF13*	16	1.70×10 <sup>7</sup>
3LF14	17	5.69×10 <sup>5</sup>

<sup>\*</sup>Runout

TABLE XIV Fatigue Data for A357-T6 at 400°F, R=0.1

PECIMEN	MAXIMUM STRESS	CYCLES
	(ksi)	
3HF1	17	5.17x10 <sup>6</sup>
CEF?	20	9.52×10 <sup>5</sup>
3HF3	25	2.01×10 <sup>5</sup>
3EF4	35	5.44×10 <sup>4</sup>
3HF5	40	1.01x10 <sup>4</sup>
3HF6 ·	45	2.00×10 <sup>2</sup>
3H <b>F</b> 7	43	2.00x10 <sup>2</sup>
3HF8	41	6.00x10 <sup>2</sup>
3HF9	41	5.80x10 <sup>3</sup>
3EF10	16	9.53x10 <sup>6</sup>
3HF11	15	6.44×10 <sup>5</sup>
3HF12	. 15	. 1.79×10 <sup>7</sup>
-3HF13	30	6.17x10 <sup>4</sup>
3HF14	37	. 1.06x10 <sup>6</sup>

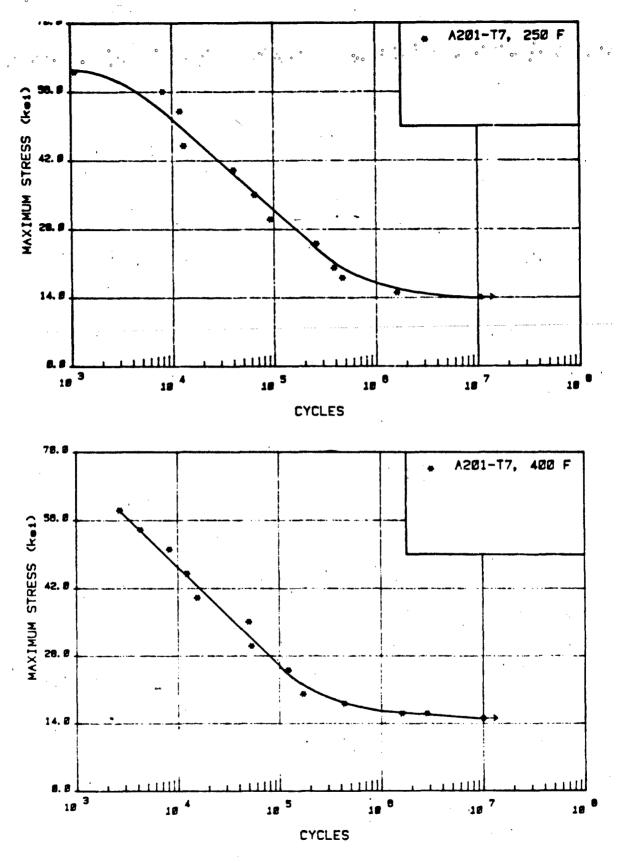


Figure 5: A201-T7 Fatigue Data, R=0.1, (a) 250°F, (b) 400°F.

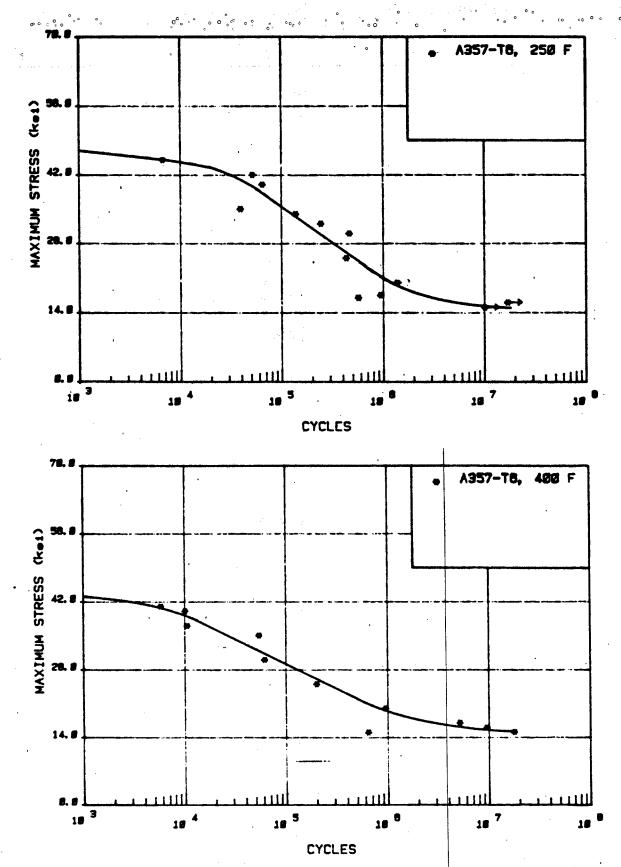
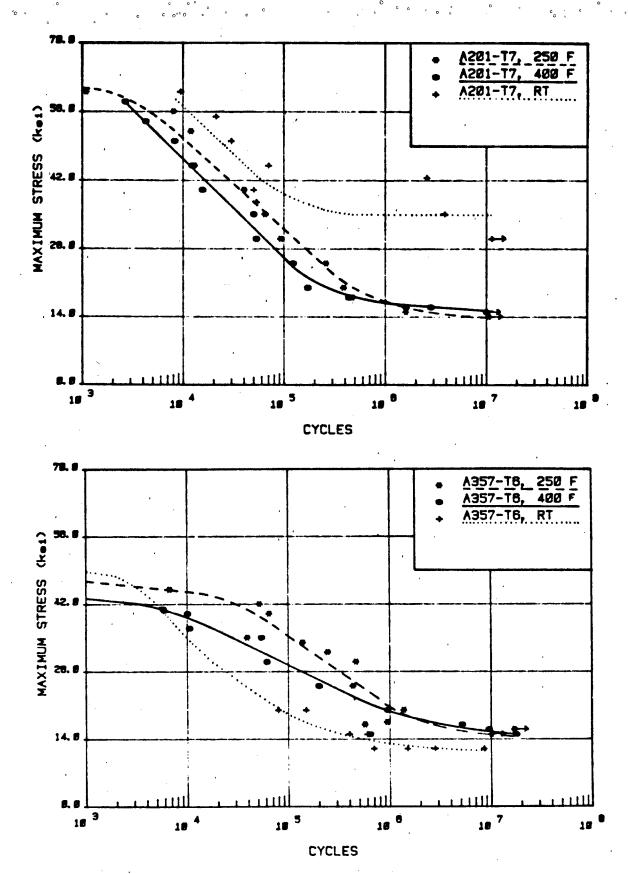


Figure 6: A357-T6 Fatigue Data, R=0.1 (a) 250°F, (b) 400°F.



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Figure 7: Combined plots of fatigue data, (a) 201-T7, (b) A357-T6.

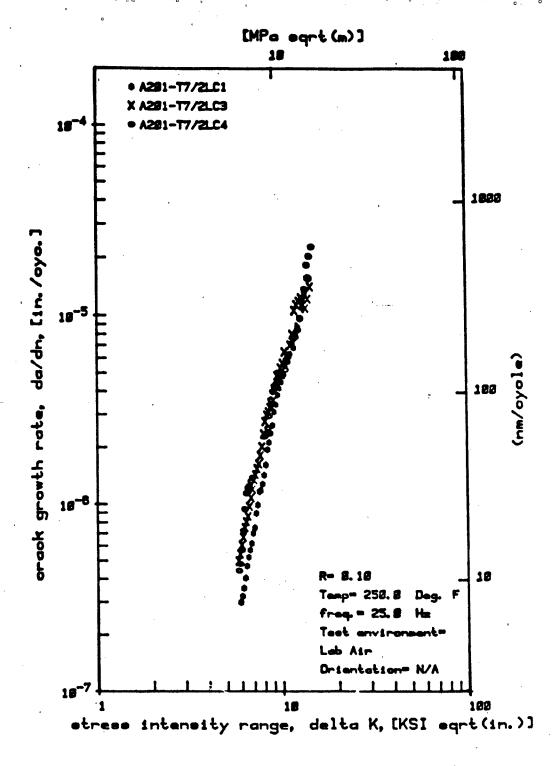


Figure 8: A201-T7 Fatigue Crack Crowth Rate Data at 250 °F.

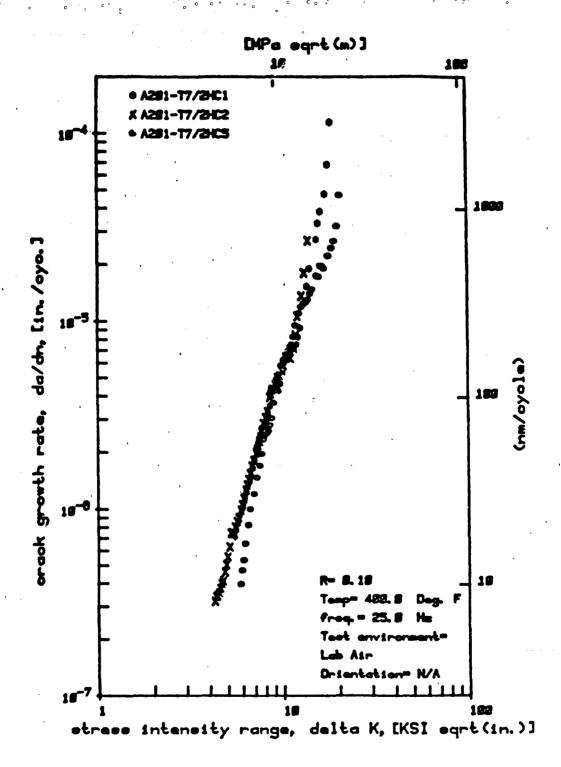


Figure 9: A201-07 Patigue Crack Growth Rate Data at 400 c.

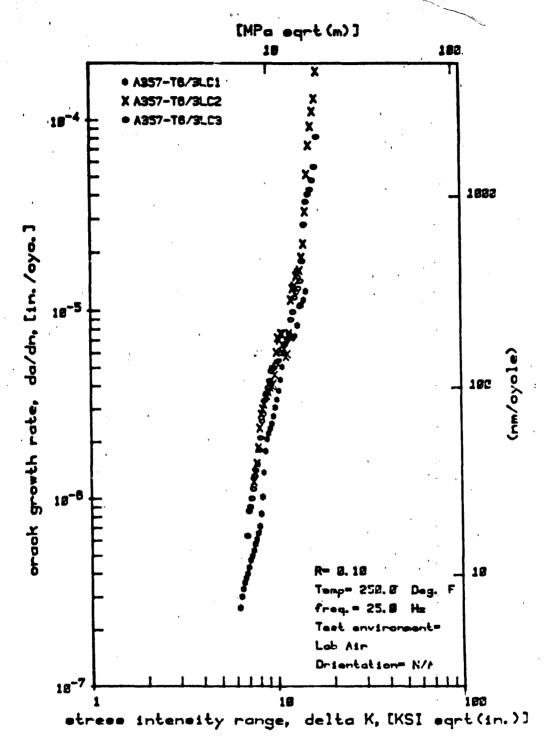


Figure 10: A357-T6 Patigue Crack Growth Rate Data at 2500c.

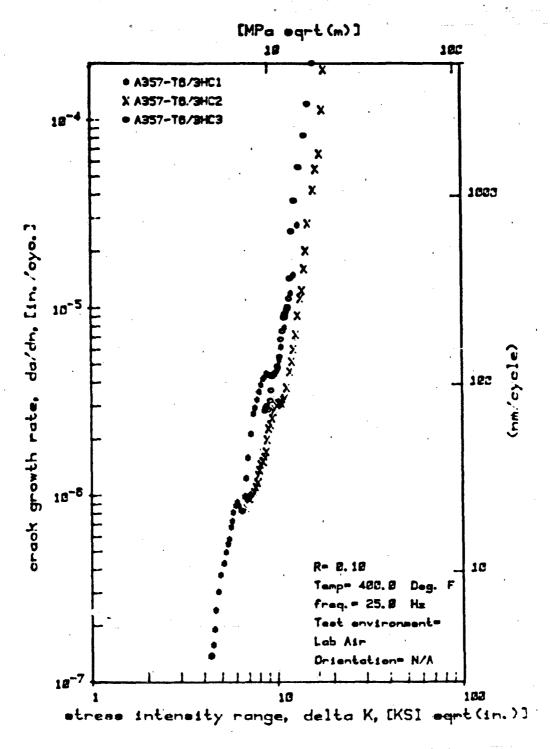


Figure 11: A357-16 Fatigue Crack Growth Rate Data at 400°F.

### SECTION IV

### **CONCLUSIONS**

# A. Tensile Properties

- 1. The ultimate tensile and yield strength of A201-T7 decreased slightly at 250°F and decreased markedly at 400°F. The percent elongation of A201-T7 increases as temperature increases.
- 2. The ultimate tensile and yield strengths of A357-T6 decrease with increasing temperature. The ultimate strength of A357-T6 at 400°F is slightly greater than the yield strength. The elongation of A357-T6 increases, then decreases, as temperature increases.
- B. Fracture Toughness Properties
- 1. The average  $K_{1c}$  for A201-T7 at 250°F is 22.3 ksi $\sqrt{1n}$ , while the average  $K_{0}$  of A201-T7 at 400°F is 25.0 ksi $\sqrt{1n}$ .
- 2. The average  $K_Q$  for A357-T6 is 27.5 ksi $\sqrt{in}$  at 250°F and decreases to 18.1 ksi/in at 400°F.
- C. Constant-Load-Amplitude Fatigue Properties
- 1. The fatigue strength of A201-T7 decreases as temperature increases from room temperature to 250° to 400°F. The fatigue endurance limit of A201-T7 at 250° and 400°F is approximately equal to 14 ksi.
- 2. The fatigue strength of A357-T6 decreases as temperature increases form 250° to 400°F. The fatigue endurance limit is approximately 15 ksi at both temperatures.

- D. Fatigue Crack Growth Rate Properties
- 1. The fatigue crack growth rate of A201-T7 increases with increasing temperature at low ranges of delta K.
- 2. The fatigue crack growth rate of A357-T6 increases with increasing temperature at low ranges of delta K.

### SECTION V

### REFERENCES

- 1. K.J. Oswalt and C. Ford, "Manufacturing Methods for Process Fffects on Aluminum Casting Allowables," Contract F33615-79-C-5116, IR 268-9(I), May 1981.
- 2. K.J. Oswalt, C. Ford, and Y. Lii, "Manufacturing Methods for Process Effects on Aluminum Casting Allowables," Contract F33615-79-C-5116, IR 268-9(II), May 1982.
- 3. J.D. Tirpak, "Constant-Load-Amplitude Fatigue Crack Growth Testing of Aluminum Casting Alloys A201-T7 and A357-T6," AFWAL-TR-85-4096, July 1985.
- 4. K.J. Oswalt and Y. Lii, "Manufacturing Methods for Process Efforts on Aluminum Casting Allowables," Contract F33615-79-C-5116, AFWAL-TR-84-4117, March 1985.
- 5. Oswalt, AFWAL-TR-84-4117, op.cit.
- 6. E.K. Gunther, "Cast Aluminum Structures Technology (CAST), Structural Test and Evaluation (Phase V), Part II-Fatigue and Fracture Properties of Cast Aluminum Bulkheads," Contract F33615-76-G-3111, AFWAL-TR-80-3021, Part II, April 1980.
- 7. O.L. Deel, P.E. Ruff, and H. Mindlin, "Engineering Pata on New Aerospace Structural Materials," Contract F33615-73-C-5073, AFWAL-TR-75-97, June 1975.
- 8. "Premium Castings-Product Manual," Aluminum Company of America, 1972.
- 9. Tirpak, op.cit.
- 10. Tirpak, op.cit.

APPENDIX

FATTGUE CRACK GROWTH RATE DATA

SPECIMEN NO.

2LC1 AUTOMATIC

Pans . 775 LBF

min = 78 LBF P = 0.30

B-0.494 in. W-1.997 in.

PT	CYCLE	A-cor	A⊣req in	<b>PC</b>	deleak KSIsin	de/de
7	CCUR:	in .	1n 	FL	NS1 <i>2</i> .E	' win/cy
			•			•
1	4.001	0.592				
2	<b>59.</b> 360	0.607	1			
3	119.490	0.622			•	•
4	175.350	0.638	0.638	0.999299	<b>5.9</b> 0	G. 2991
5	219.800	4.653	0.652	0.999295	6.02	6.3221
6	273.140	0.668	0.670	0.999186	6.13	0.3566
7	312.310	0.684	0.683	0.997877	6.26	0.4052
	350.040	Q.699	0.699	0.998766	6.38	0.4593
• •	384.920	0.714	0.716	0.998586	6.51	0.5224
10	408.89Q	0.730	0.729	0.998781	6.64	0.5698
11	433.860	0.745	0.744	0.998920	6.77	G.6180
12	460.840	0.760	0.761	0.996632	6.91	0.7001
13	401.710	0.776	0.776	0.997739	7 0 !	0.7478
34	503.540	4.791	0.793	0.993495	7.19	0.8936
15	515.650	0.806	0.804	0,993358	7.34	0.9900
16	537.530	0.822	0.827	0.993870	7.50	1.1661
17	543.610	Q.837	0.834	0.993189	765	1.1819
18	557.900	0.053	0.852	0.993457	7.82	1.2763
19	569.350	0.868	0.868	0.992763	7.96	1.4231
20	582.020	0.883	0.885	0.997968	B.15	1.6117
21	591.310	0.899	0.900	0.997926	8.33	1.9454
22	590.330	0.914	0.914	0.997982	8.51	2.1265
23	605.320	0.929	0.930	0.998380	8.69	2.3772
24	610.420	0.945	0.942	0.997328	8.90	2.6182
25	617.690	0.960	0.962	0.995875	9. 10	3.0987
26	623.290	0.975	0.976	0.996263	9.30	3.3793
27	626.460	0.991	0.990	0.997490	9. !3	3.8218
28	629.650	1.006	1.004	0.998219	9.76	4.1368
29 ,	634.150	1.021	1.024	0.998248	9.99	4.4494
30	636.840	1.037	1.035	0.996597	10.25	4.8524
31	64C.270	1.052	1.052	0.997430	16.50	5,4990
32	643.310	1.067	1.070	0.996462	10.76	5.8547
33	645.280	1.083	1.001	0.996873	11.05	6.1330
34	647.490	1.098	1.096	0.995836	11.34	6.7893
35	650.46C	3.114	1.117	0.995628	11.66	7.5452
34 37	652.310	1.129	1.130	0.997922	11.97	€.0631
37	653 730 655.670	1.144	1.142	0.998209	12.30	6. <b>67</b> 62
39	657 310	1.16C 1.175	1.160	0.998996	12.67	(,6395
40	658.630	1.175	1.176	0.996140	13.04	16.9331
41	660.000	1.190	1.190	0.996123	13.42	13.0224
42	664.770	1.221	1.209	0.997572	13.84	15.6550
4.3	€C690	1.236	1.221	0.993170	14.27	15.6281
44		1.752				
45	14 340	1.247	•			

EFECIPEN NG.

2LC 3 AUTOMATIC

BAR . ROO LBF

PRID . 80 LEF . . C. 100

B=0.492 in. W=1.998 in.

PT	CYCLE	A-ccr	A-st eg	_	delter	đa/cn .
•	COUMS	.in	in	₩C	RS1¢'5	win/cy
						,
1	0.001	0.549				
:	'46.8 C	0.564				
3	93.2 0	0.560				0.4981
4	126.6 C	0.595	0.596	0.999288	5.79	0.4981
5	152.7.0	0.611	0.610	0.999110	5.91	0.6050
6	101.4 0	Q.626	0.626	8.999249	6.02	0.6647
7	204.110	Q.641	0.640	0.998578	6.14	0.7494
. 8	236.630	4.657	0.658	0.999444	6.27	0.8044
9	248.970	0.672	0.672	0.999258	6.39	0.7974
10	265.630	Q.687	0.687	0.995628	6. 51	
11	283.150	0.703	0.703	0.980439	6, 65	0.9001
12	300.630	0.718	0.718	0.973364	6.78	1.0231
13	324.740	0.733	0,744	0.974707	6.91	1.3253
14	324.740	0.749	0.743	0.977720	7.06	1.3826
1.5	337.410	G.764	0.762	0.971364	7.70	1.4946
16	347.800	0.779	0.781	0.977246	7.34	1.6676
17	354.93G	0.795	0.791	0.995954	7.49	1.6280
18	367 € 70	0.810	0.813	0.496004	7.64	1.8045
19	374.210	0.825	0.825	0.993864	7.80	2.0143
20	381.670	0.841	0.839	0.996179	7.97	2.3561
21	389.700	0.856	0.860	G. 996136	8.13	2.7451
2.3	393.850	G.872	0.871	0.997:45	B.31	2.9807
23	39B.2HU	0.897	0.885	0.995207	8.49	3.0960
24	403.460	0.902	0.904	, 0.999169	8.67	3.7634
25	407.590	0.918	0.916	0.997932	8.67	3.2872
26	412.946	0.933	0.933	0.997087	9.06	3.5478
27	417.690	0.948	0.950	0.996998	9.26	4.0431
:8	421.150	. 0.964	0.964	0.998181	9.48	4.8254
29	424.30L	0.979	0.980 .	0.991814	9.70	4.9628
30	427.060	0.994	0.995	0.993555	9,92	5.3126
31	426.940	1.010	1.005	0.991808	10.17	5.6197
3.2	433.190	1.075	1.079	0.990352	10.41	6.4514
3.3	434.97	1.040	1.041	G. 98644E	10.67	6.1632
34	437.070	1.056	1.054	8.987065	10.95	6.2171 7.0077
35	438.810	1.071	1.067	0.969936	11.22	7.,9697
36	442.250	1.086	1.089	0.986771	11.51	10.6003
37	444.310	1.102	1.105	0.988550	11.63	11.3675
38	445.610	1.117	1.110	0.991367	12.14	11.6114
39	446.520	1.133	1.130	6.991990	12.49	12.3366
40	447.640	1.148	1.147	0.997982	12.84	11.3359
41	449.170	1.163	1.164	0.994791	13.20	10.9097
42	450.440	1.179 .	1.176	0.992258	13.60	12.1749
43	452.570	1.194	1,198	0.994146		14.0806
44	453.510	1.709	1.209	0,994600	14.42	10.0000
45	454.4+0	1.175				
46	455,570	1.240		•		
47	456.130	1.255				

EPECIMEN NO.

STC3 MANCAT

Pmes = 800 LPF Pmin = 80 LBF P

B=G.492 in. W=1.998 in.

77	CYCLE	A-cor in	Anleg in	MC	deltek KSI4in	da/ón uin/cy
1	6.001	0.548	•		•	
2	55.000	0.574				•
3	100,000	0.586			• .	
ă	140.000	0.619	0.615	0.992881	5.97	0.6406
Š	170.0.0	0.633	0.634	0.994617	6.08	0.7363
í	200.0	0.654	0.658	0.995623	6.24	0.8369
ž	225.0 0	0.681	0.679	0.995856	6.46	0.8780
á	250.0:0	0.704	0.703	0.998249	6.66	0.9363
•	270.010	0.724	0.723	0.998776	6.83	0.9708
<b>J</b> Ó	290.0:0	0.740	0.741	0.998570	6.97	1.0197
ii	310.010	0.761	0.761	0.998262	7.17	1.1581
12	325.000	0.778	0.778	0.999784	2.33	1.3033
13	340.010	0.798	0.799	0.999010	1.52	1.5314
34	355.010	ù.823	0.823	0.999292	7.78	1.7463
15	370.010	0.849	0.851	0.999262	8.06	1.9995
16	340,636	G.874	0.872	0.999141	8.34	2,1598
17	396.630	6.893	0.872	0.998405	8.56	2.1598
jé	395.636	0.906	0.406	0.997642	8.72	
19	406.000	6.918	0.406	0.999731	8.87	2.5789
20	405: (00	0.934	C.933	0.999731	9.08	2.7978
21 .	416.600	0.949	0.950	0.999368	9.28	3.1500
22	415.000	Q.967	0.968	0.999388		3.4357
23	420.000	0.989		0.999478	9.53	3.7698
24	425.000	1.008	0.987	0.999540	9.85	4.1086
25	428.000	1.022	1.022	0.999443	10.14 10.37	4.4184
26	431.000	1.027	1.034	0.998035	16.62	
27	434.000	1.051	1.051	0.998355	10.86	5.1170
28	437.000	1.067	1.069	0.998447	11.15	. 5.7071 6.5524
29	439.000	1.084	1.082	0.999029	11.47	7.1927
30	443.000	1.112	1.114	0.998206	12.04	8.4126
31	445.000	1.133	1.132	0.990261	12.49	8.6680
32	446.500	1.147	1.145	0.997759	12.81	8.7496
33	449.000	1.158	1.159	0.997647	13.08	4.1841
34	449.500	1.172	1, 171	0.997005	13.42	9, 77 29
35	451.000	1.185	1.186	0.998763	13.76	11.0946
36	452.500	1.202	1.204	0.996177	14.23	13.9873
37	453.100	1.216	1.216	0.991330	14.69	14.2120
38	454.700	1.232	1.232	0.987279	15.11	14.4928
39	455. 00	1.741	1.246	0.982879	15.39	16, 1018
40	456. 00	1.769	1.262	0.981539	16.34	18.1135
41	458. 00	1.283	1.292	0.968876	16.85	28.2780
42	458. 00	1.304	1.305	0.972851	17.66	35.4830
4.3	454. 00	1.316	••••	· · · · · · · · · · · · · · · · · · ·		33,40.0
4.4	459. 00	1.350				
45	454. 90	1.363				

22 314.5 3484

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. PT	CYCLF	A-ccr	A-1100		delter	da/cr
	COUNT	- in	1 n	PC	REIS:R	#14/c}
3	0.001	0.804		•		
2	2.310	0.819	•	*		•
ž	13.500	0.835			8.08	2,3457
Ä	19.320	4.850	0.848	0.997903	8.61	2,8785
5	40.460	0.896	0.899	0.996199	8.81	3,5068
6	45.360	.0.912	0.912	0.997932	9,00	3,9334
7	49.800	0.927	0.924	0.999840		4,1506
Š,	53,250	4.942	T.942	0.499062	9.20	4.7181
•	59.990	0.973	0.972	0.998989	9.63	4.8519
10	62.960	0.988	0.987	0.999159	9.85	4,9375
îĭ	66.010	1.004	1,006	0.999147	10.10 10.34	5,1027
12	69.040	1.019	1,017	0.998146		5.2917
13	72.270	1.034	1.034	0.998315	10.59	6, 1316
14	78.390	3.065	1.067	0.997016	11.13	6.6794
15	80.270	1.680	1,078	0.998881	11.42	7,8343
16	83,140	1,096	1.098	0:997870	11.73	8.3159
37	84.670	1.111	1,109	b.998302	12.04	10.5949
16	88.490	3.142	1.144	0.995182	12.72	13.3316
19	90.980	3.173	1.172	0.996634	13.48	16.8559
20	92.420	1.180	1,193	0.993153	13.87	19.7414
21	93.140	1.203	1,205	0.993840	14.:8	
22	93.940	1.219	1,220	0.995627	24.75	22.697
23	94.350	3.234				
24	95.150	3.750				
25	95.680	1,265				

EFICINEN NC.

2LC4 PINLAL

Pes> - 800 LbF

£=0.491 in. h=1.998 in.

rt	CYCLI	A-cce	Amira		ccltet	. ca/dr
•	COUNT	ni.	in	PC	K5) <= r	win/cv
)	0.001	0.548				
2	30.000	0.561				
3	120.400	0.811				
4	150.000	0.625	0.627	Q.99H657	6.13	0.6420
5	180,000	0.647	0.649	0.998548	6.20	0.7610
•	210.000	0.674	0.672	0.998822	6,42	0.6680
7	235.000	4.695	0.695	0.998995	6.59	0.9756
	250.000	4.708	0.710	0.998719	6.71	1.0645
•	245.000	0.726	0.726	8.999504	6.86	1.1361
10	280.000	4.744	0.744	0.999246	7.02	1.2119
11	295.000	0.764	0.763	0.599244	7.21	1.3062
12	310.000	0.783	0.783	0.998438	7.39	1.4215
13	325.000	0.802	0.804	0.998452	758	1.6167
14	335.000	0.820	0.820	0.999639	7.,76	1.7800
15	345.000	0.839	0.838	0.999673	7.96	2.0086
16	355.000	0.860	0.860	0.999686	8.19	2. 2620
17	365.000	0.882	0.883	0.999746	8.45	2,5403
10	375.000	0.910	0.910	0.999849	8.79	2.8807
19	382,000	0.930	0.730	0.999619	9.04	3.2610
20	387000	0.947	0.947	0.999591	9.27	3.5404
21	390.000	0.957	0.957	0.999673	9.41	3.7731
22	395.000	0.978	0.977	0.999297	9.70	4.2770
23	400.000	0.998	0.999	0.999661	10.01	4,8504
24	405.000	1.024	1.025	0.999228	10.42	5.3840
25	410.000	1.055	1.053	0.998542	10.95	6.1534
26	414.000	1.080	1.078	0.995834	11.42	3.3424
27	410.000	1.103	1.100	0.996613	11.87	8.4498
20	421.000	1.132	1.173	0.998204	12.50	10.1117
29	424.000	3.167	1.165	0.998479	12.33	12.5616
30	426.000	1.188	1.193	u.995576	13.87	15.0250
31	427.000	1.206	1.210	0.983829	14.37	20.6029
32	427.500	1.716				
33	428.000	1.229				
34	428.500	1.251				

SPECIMEN NO.

2HC1 MANUAL

Pres = 7.00 LBP

Pain - 70 LBF

P - 0.10G

B-0.494 in. N-2.053 in.

pt	CYCLE	A-cor .in	A-reg	, NC	deltak KSlyin	de/dn win/cy
	-i-airioreses -com					
•						
1	0.001	0.561 0.580		•		
3	35.000	Q.596				
3'	65.000 95.000	0.611	0.612	0.999424	4.97	0.5814 0.6196
.5	125.000	0.629	0.629	0.999770	5.09 5.20	0.6539
	150.000	0.646	0.645	0.999717	5.20	0.6637
7	170.000	0.659	0.659	Q.999596 Q.999245	5.37	0.6881
i	190.000	0.673	0.673 0.686	0.999227	5.47	0.7107
	210.000	0.687	0.700	0.998384	5.55	0.7714
10	230.000	9.699 9.716	0.716	0.999172	5.67	0.8367
11	250.000	0.732	0.733	0.999220	5.79	0.9165
12	270.000 290.000	0.754	0.753	0.999512	5.95	0.9975 1.0511
14	305.000	€.768	9.768	0.999506	6.05 6.18	1.1301
15	320.000	0.784	0.784	0.998757	6.31	1.2366
16	335.000	0.473	0.801	0.999608 0.999623	6,46	1.3644
17	350.000	0.813	0.820 0.834	0.999541	6.60	1.4402
18	360.000	0.835	0.850	0.999385	6.73	1.4950
19	370.000	Q.850 Q.865	0.864	0.996988	6.86	1.6393
20	300.000	0.881	0.880	0.997655	7.01	1.7935 2.0684
21 22	390.000 400.000	0.896	0.899	0.998446	7.15	2.3559
23	410.000	0.921	0.920	8.998354	7.39 7.52	2.4940
24	415.000	0.933	0.932	0.998110 0.998791	7.66	2.6921
25	420.000	0.947	0.946	0.997928	2.78	2.7143
26	425.000	0.950	0.960 0.973	0.997961	2.95	2.8429
27	430.000	0.973 0.990	0.988	0.997855	8.15	2.9979
28	435.000	1.001	1.003	0.997562	6.78	3.2393
29 30	440.00 <i>0</i> 445.000	1.019	1.019	0.997980	8.50	3.5321 4.3402
31	448.000	1.030	1.029	0.992854	8.64	4.7102
32	451,000	1.042	1.044	0,979399 0,982323	8.80 8.96	4.3767
33	454.000	1.054	1.050	0.984021	9,34	4.4287
. 34	457.000	1.000	1.072 1.097	0.981757	9, 53	4.2475
35	463.000	1.093 1.107	1.109	0.977700	9.75	4.6426
36 37	466.000 469.000	3.122	1.121	0.999209	9.99	5.4801
38	471.000	1.132	1.133	0.999495	10.16	6.0375 6.4326
39	473.000	1.146	1.146	0.999264	10.41 10.66	6.9464
40	475.000	1.160	1.159	0.999429 0.999723	10.93	7.3214
41	477.000	3.174	1.174 1.169	0.998361	11.20	7.2500
42	479.000	1.188 abox	1.204	0,998569	11.56	2.1607
43	481.(00		1,218	0.994887	11.88	7.4821
44	483.100		1.232	0.992193	.12.13	8.2455 9.2293
45	465.00C 487.00C	3.745	1.248	0.996939	12.47 13.02	12,4107
46 47	489.000	1.267	1.266 1.285	0.992675	13.56	15.3625
48	440,500	4.401	1.310	0.994626	14.02	19.0262
49	492.000	1.303	1.341	0.992661	15.29	27.2023
50	493.500	1.343 1.353	1.354	0.994840	15.64	33.2106
51	494.000	1.366	1.372	0.993582	76.11	38.4982 47.8503
52	494,500 495,000	1.392	1.390	0.998023	12.14	48.4047
53 54		1.406	1.405	0.973303	17.73 18.41	114.2865
55		1.421	1.427	0.935623		
56		1.435				
57	496.000	3.474				
58	496,100	1.510			•	•

## 6 AUGUST 1984

SPECIMEN NO. 2NC: AUTGMATIC

Page - 600 LBF Pair - 60 LBF R = 0.300

B-G.494 in. W-2.052 in.

PT	CYCL!	A-cor	Anies in	нс	deltek ESIdin	de/dn win/cy
1	4.001	0.556			t	
2	42.530	0.573				
3	93.210	0.588				
•	143.710	0.604	0.605	0.999533	4.23	0.3325
5	187.150	9.619	0.619	8.999649	4.31	0.3372
	272.230	0,650	0,649	0.999725	4.40	0.3500
7	319.970	0.665	0,666	D.999776		0.3545
•	358.870	0.680	0.480	0.999724	4:65	0.3585
•	405.410	0.696	0,696	0.999306	4.74	0.3748
10	445.470	0.711	0.711	0.999297	4.03	0.3967
11	485.600	Q,726	0.726	<b>0:99</b> 7207	€.93	0.4576
12	517.940	0.742	0,741	0.998268	5.03	0.5177
13	552.420	0,757	0,750	0,998839	5.12	8.5908
34	594.710	0.788	0.787	D", 998388	5.33	0.6785
15	615.450	0.803	0,802	0:997759	5.43	0.7432
16	638.400	0.819	0.820	0.997922	5:54	0.8073
17	659.330	0.834	0.836	0.998466	5.65	0.8576
18	671.990	0.849	0,847	0.998523	5.76	0.9096
19	609.720	0.865	0.864	0.997450	5.88	1.0217
20	706.490	0.880	0.361	0.994632	6.00	1.2045
21	719.920	0.896	0.897	0:998222	6.13	1.3882
22	729.680	0,911	0.912	0.996682	6.26	1.4686
73	737.800	0.927	0.925	0.498003	6.40	1.5650
24	742.760	0.942	0.941	0.998496	6.53	1.6606
75	758.670	0.958	0.959	0.996749	6.68	1.8004
26	766.960	6.973	0.974	0.996644	6.02	1.9190
27	774.510	G.9H8	0.929	0.99941	6.97	2.1628
28	780.580	1.004	1.007	0.999671	3.12	2,2349
29	780.330	1.019	1.620	0.99916(	, 3.29	2.3717
30	793.760	1.034	1.034	0.99822	2.45	2.3531
21	80Q.3' C	1.050	1.050	8.398201	3.64	2.3118
32	804.24C	3.065 ·	1.064	0.598946	7.82	2.3335
33	614.1 0	1,000	1.01	0.51977:	6.01	2,4648
34	F21.6 0	1.096	1.197	0.563245	8.77	3.1645
35	923.4 (	1.331	1,116	0.069303	8.42	4.2772
36	429.1 A	1,126	1.127	0.966743	8.63	4.2705
37	432.1 0	1.14;	1.170	6.446614	8.27	4,1907
38	535 . 6 70	1.317	1,71:	C.5 25 6.21	9.10	5.1377
2 :	30 .1 1h	1.17;	1.174	<b>(, տ</b> փ ֆ( ևտ	9.35	5.41%
40	142.1;0	1.1/2	1.1)1	0.594572	9.17	5.7047
41	37.3 . 0.20	1.203	1.240	0.001 334	9.87	5.5727
47	84646	1.219	1.410	n, star in	16.10	5. (**
4.7	44710	3-424		•		
4.6	A52.+16	1.79	•			
4 4	854. VII	3.265				

## 6 AUCUST 1984

BPLCIPEN NG.

THEZ MANLAL

Pres . 600 LHF

841 24 e e

F . C.10C

B-0.494 in. h-2.057 in.

<b>P</b> 7	CYCL F COUNT	A-cot	A-1eq in	ис	deltek KSly:n	da/dn
	COUNT		*******	nc	#215.A	-uin/cy
						,
3	0.001	0.558				
2	60.000	0.569				
4	120.000 160.000	0.55î 6.59ê	0.595	0.998610	4.18	
	200.000	0.607	0.667	0.596503	4.14	0.2854 0.3198
:	240.000	0.620	0.621	0.998067	4.31	0.3384
7	200.000	0.633	0.634	0.997868	4.38	0.3446
i	320.000	0.651	0.649	0.998530	4.48	0.3557
•	366.000	0.663	0.663	0.996987	4.55	0.3753
10	400.000	0.677	0.678	0.996988	4.63	0.3961
11	435.000	0.490	0.691	0.998838	4.71	0.4122
12	470.GCC	0.709	0.706	0.99H397	4.82	0.4621
13	500.000	0.721	0.721	0.998405	4.89	0.5050
14 15	530.000	0.734	0.736	0.998349	4.98	0.557
16	560.000 585.000	0.754 0.769	0.753	0.999380	5.10	0.6301
17	610.000	0.787	0.77u 0.78 <b>6</b>	0.998950 0.999335	5.20 5.32	0.6870 0.7476
10	635.600	0.809	0.807	0.999307	5.47	0.8051
19	640.000	0.877	0.828	0.999383	5.60	0.8655
20	680.000	0.845	0.846	0.999285	5.73	0.9013
21	700.000	0.865	0.864	0.998650	5.88	0.9895
23	715.000	0.279	0.679	0.998754	5.99	1.0582
23	730.00C	0.893	0.895	G.99F771	6.11	1.1406
24	745.000	0.914	0.412	0.999154	6.28	1.2556
3.5	755.000	0.925	0.925	0.999143	63b	1.3361
26 27	765.000	0.939	0.939	0.999240	6.50	1.4298
28	775.000 785.000	0.954 0.969	0.953 0.969	0.999580	6.64	1.5293
29	795.000	0.986	0.967	Q.9995H3 Q.999364	6.78 6.95	1.6874
30	805.000	3.007	1.004	0.999166	3.17	1.8073
31	810.00C	1.016	1.016	0.999113	76	2.0862
32	815.000	1.025	1.027	0.996998	7.36	2.1734
33	820.00C	1.038	1.637	G.999162	7.51	2.2883
34	<b>8</b> 27.000	1.054	1.054	0.999218	7.69	2.5957
35	<b>6</b> 32.000	1.066	1.067	0.999254	7.84	2.8529
36	837.000	1.002	1.082	0.999680	B.04	3.0775
37 38	842.000 847.000	1.098	1.098	G. 999389	8.75	3.2936
39	850.000	1.116 1.126	1.115 1.127	0.993486 Q.993644	8.49	3.9303
40	853.000	1.136	1.140	0.993830	B.63 B.78	4.0839 4.3362
41	856.000	1.158	1.153	0.994109	9.12	4.6032
42	060.500	3.174	1.175	0.994395	9.38	5.6114
43	863.500	1.190	1.191	0.994267	9.65	5.1152
44	866.500	3.705	1.205	0.998230	9.92	5.4454
45	868.000	1.216	1.214	0.998181	16.12	1.8212
46	871.00C	1.130	. 231	0.997879	10.40	6.5012
47	874.000	1.251	4.253	0.490966	. 10.83	6.4401
46	e75.500	3.763	1.263	0.990562	11.09	6.3869
49	877.500 886.500	1.261	1.276	0.976217	11.50	7.1767
50 51	8P2.(00	1,292 1,303	1.307	0.978791 0.964092	11.76 12.04	8.4476
52	863.500	1.327	1.323	0.995953	12.67	10.6367 13.6496
53	885.000	1.342	1.346	0.993972	13.10	18.1133
54	886.000	1.364	1.364	0.965094	13.77	26.5601
5 4	887.660	1.385		2.2.2.74		••••••
56	867.500	1.403				
57	9 e B . 00 C	1.445			4	

10 AUGUST 1984

SPECIMEN NG.

THES MARUAL

The BO FRE P. C. 100

5-G.495 in. 'bel.499 in.

PT	CYCLE	A-cor in	A-neg ir	MC	deltak #Sluin:	da/dn win/cy
	•••••			•••••••		
1	0.001	0.565				
2	40.000	0.577				
3	80.000	0.591				
4	120.000	0.608	0.607	0.999543	5.85	0.3966
5	155.000	0.622	0.621	0.991956	5.95	0.4702
6	190.000	0.637	0.637	0.994319	6.07	0.5333
7	225.00C	0.652	0.655	0.995305	. 6.19	0.6547
•	260.00C	G. 684	0.680	0.997127	6.45	0.0233
9	290.00C	0.702	0.706	0.997795	6. AC	3.0002
١٥.	320.000	0.739	0.739	8.997598	6.92	1.2082
11	345.000	0.770	0.769	0.998645	7.:0	1.4687
2	365.000	0.799	0.802	0.998059	7.48	1.6976
3	375.000	0.817	0.519	0.999347	7.66	1.9640
4	382.000	0.033	0.033	0.997996	7.83	2.3415
15	38700C	0.844	0.844	6.99(874	7.95	2.4652
6	392.00C	0.855	0.856	0.994074	8.07	2.4885
7	397.000	0.874	0.871	0.994352	8.18	2.5500
8	402.00C	0.884	0.8F3	0.994419	6.29	2.6286
9	467.600	0.094	0.896	0.99:363	8.53	2.8000
0	412.GOO	6.909	0.908	G. 999585	8.69	3.6420
1	417.00C	0.924	0.924	0.599484	8.66	3.665
2	422.000	0.944	0.944	0.999212	9.14	4.491
3	425.000	0.957	0.956	0.999433	9.32	4.931
4	431.000	6.990	0.996	0.998916	9.79	5.807
25	434.600	1.011	1.009	0.997891	10.12	6. 219.
20	436.000	1.022	1.C22	G.94A759	10.29	6.769
27	438.000	1.023	1.035	0.098342	10.47	6.403
28	440.000	1.049	1.047	0.99+752	10.75	6. 517
9	442.000	1.060	1.061	0.998939	10.94	6. 829
30	444.001	1.074	1.074	0.996713	11.26	7.517
11	446.000	1.089	1.088	0.999679	.11.4ê	8.275
32	445.000	1.104	1.106	0.999257	11.78	5.527
33	450.00C	3.147	1.126	0.594462	12.27	11.054
4	451.50C	1.143	1.143	0.998873	12.63	11.935
35	453.000	1.162	1.163	0.999255	,13.CB ,	12.499
6	454.000	1.177	1.175	0.999636	13.45	12.675
17	455.000	1.188	1.108	0.999373	13.74	13.073
16	456.000	1.201	1.201	0.997670	14.09	13.477
9	457.000	1.214	1.213	0.997921	14.46	14.270
G	459.000	1.742	1.245	0.996013	15.31	16.198
11	459.500	1.254	1.254	0.598141	15.70	19.219
12	460.000	1.265	1.263	0.998199	16.07	20.607
13	460.500	1.275	1.275	0.997878	16.43	21.795
14	461.000	1.784	1.206	0.996185	16.76	21.504
<b>4</b> 5	462.000	1.310	1.307	0.997035	17.77	22.310
6	463.000	1.326	1.330	0.996783	18.53	24.551
47	463.50C	1.340	1.342	0.946291	19.07	26.707
18	454.000	1.356	1.354	G. 935510	19.84	32.061
49	464.500	1.376	1.366	0.962024	20.54	47.003
50	465.000	1.387				
5 1	465.500	1.417				
5 2	465.800	1.469				

## 6 SE 17 198

SPECIMEN NO.

SMC1 AUTOMATIC

PRAS . 850 LBT

eir = #5 LbF F = 0.10

p.5.473 in. N=3.050 in

\$ CCUNT IN MC #51&F  1 0.001 0.555 2 127.470 0.571 3 205.780 0.586 4 268.050 0.602 0.611 0.999850 6.25 5 324.700 0.617 0.617 0.99850 6.37 6 372.900 0.632 0.633 0.999702 6.49 7 416.460 0.688 0.648 0.999714 6.62 8 455.780 0.663 0.663 0.663 0.999787 6.74 9 496.950 0.663 0.663 0.663 0.999787 6.76 9 496.950 0.663 0.679 0.999787 6.76 10 533.910 0.694 0.679 0.999783 6.87 10 533.910 0.694 0.679 0.999783 7.01 11 571.600 0.709 0.710 0.999310 7.14 12 602.880 0.724 0.725 0.998935 7.28 13 628.996 0.740 0.738 0.998784 3.63 14 657.830 0.755 0.754 0.998837 3.57 15 667.410 0.770 0.772 0.998860 3.71 16 709.816 0.786 0.785 0.999293 7.87 17 732.130 0.801 0.800 0.999306 8.02 18 755.046 0.817 0.99328 8.35	-uin/cy
2 127.470	·
2 127.470	
3 205.780	
4 268.050 0.602 C.601 0.999950 6.25 5 324.700 0.617 0.617 0.99950 6.37 6 372.900 0.632 0.633 0.999702 6.49 7 416.460 G.648 0.648 0.999714 6.62 8 455.780 0.663 0.663 0.999787 6.74 9 496.950 G.678 0.679 0.999787 6.74 10 533.910 0.694 0.693 0.998949 7.01 11 571.600 0.709 0.710 0.998949 7.01 12 602.880 0.724 0.725 0.998935 7.28 13 628.990 0.740 0.738 0.998787 3.63 14 657.830 0.755 0.754 0.998837 3.57 15 687.410 0.770 0.772 0.99880 3.71 16 709.816 0.786 0.785 0.9999316 3.87 17 732.130 0.801 0.800 0.999316 8.18	
\$ 324.700 0.617 0.617 0.999830 6.37 6 372.900 0.632 0.633 0.999702 6.49 7 416.460 0.648 0.648 0.999714 6.62 8 455.780 0.663 0.663 0.999718 9 496.950 0.678 0.679 0.999753 6.87 10 533.910 0.694 0.693 0.998949 7.01 11 571.600 0.709 0.710 0.999710 7.14 12 602.880 0.724 0.725 0.998935 7.28 13 628.990 0.740 0.738 0.998784 3.63 14 657.830 0.755 0.754 0.998837 3.57 15 687.410 0.770 0.772 0.998807 3.57 15 687.410 0.770 0.772 0.99880 3.7 17 732.130 0.801 0.800 0.999300 8.02 18 755.046 0.817 0.8996198 8.18	0 3636
6 372,900 0.632 C.633 0.999702 6.49 7 416.460 0.648 0.648 0.999714 6.62 8 455,78C 0.663 0.663 0.999715 6.74 9 496.950 0.678 0.679 0.999753 6.87 10 533,910 0.694 0.693 0.998949 7.01 11 571.600 0.709 0.710 0.999710 7.14 12 602.88C 0.724 0.725 0.998935 7.28 13 628.990 0.740 0.738 0.998784 3.43 14 657.830 0.755 0.754 0.99837 7.57 15 687.410 0.770 0.772 0.998837 7.57 15 687.410 0.770 0.772 0.998860 3.71 16 709.816 0.786 0.785 0.999293 7.87 17 732.130 0.801 0.800 0.999306 8.02 18 755.046 0.817 0.996198 8.18	0.2626 0.3023
7 416.460 G.648 O.648 O.999714 6.62 8 455,78C O.663 O.663 O.999787 6.74 9 496.950 G.678 O.679 O.999753 6.87 10 533,910 G.694 O.693 O.998949 7.01 11 571.600 O.709 O.710 G.999310 7.14 12 602.88C O.724 O.725 G.998935 7.28 13 628.99G O.740 O.738 G.998784 3.43 14 657.830 G.755 O.754 G.998837 3.57 15 687.410 G.770 O.772 G.998860 3.71 16 709.81G O.786 O.785 G.999293 7.87 17 732.130 G.801 O.800 G.99930G 8.02 18 755.04G G.916 O.817 G.996196 8.18	0.3307
7 416.460 G.648 O.648 O.999714 6.62 8 455,78C O.663 O.663 O.999787 6.74 9 496.950 G.678 O.679 O.999753 6.87 10 533,910 G.694 O.693 O.998949 7.01 11 571.600 O.709 O.710 G.999310 7.14 12 602.88C O.724 O.725 G.998935 7.28 13 628.99G O.740 O.738 G.998784 3.43 14 657.830 G.755 O.754 G.998837 3.57 15 687.410 G.770 O.772 G.998860 3.71 16 709.81G O.786 O.785 G.999293 7.87 17 732.130 G.801 O.800 G.99930G 8.02 18 755.04G G.916 O.817 G.996196 8.18	
8 455,78C 0.663 0.663 0.99787 6.76 9 496,950 0.678 0.679 0.999753 6.87 10 533.910 0.694 0.693 0.998949 7.01 11 571.600 0.709 0.710 0.999310 7.14 12 602.88C 0.724 0.725 0.998935 7.28 13 628.990 0.740 0.738 0.998784 3.43 14 657.830 0.755 0.754 0.99837 3.57 15 687.410 0.770 0.772 0.998837 3.57 15 709.816 0.786 0.785 0.999293 7.87 17 732.130 0.801 0.800 0.999306 8.02 18 755.046 0.817 0.996198 8.18	0.3578
10 533.910 Q.694 Q.693 Q.998949 7.01 11 571.600 Q.709 Q.710 Q.999310 7.14 12 602.880 Q.724 Q.725 Q.998935 7.28 13 628.990 Q.740 Q.738 Q.998794 3.49 14 657.830 Q.755 Q.754 Q.998837 7.57 15 687.410 Q.770 Q.772 Q.998860 7.71 16 709.810 Q.786 Q.785 Q.999293 7.87 17 732.130 Q.801 Q.800 Q.999300 8.02 18 755.046 G.816 Q.817 Q.996198 8.18	0.3785
11 571.600 0.709 0.710 0.999310 7.14 12 602.880 0.724 0.725 0.99835 7.28 13 628.990 0.740 0.738 0.99878 7.25 14 657.830 0.755 0.754 0.998837 7.57 15 687.410 0.770 0.772 0.998860 7.71 16 709.810 0.786 0.785 0.99929 7.87 17 732.130 0.801 0.800 0.999306 8.02 18 755.046 0.817 0.996198 8.18	0.4008
12 602.880 0.724 0.725 0.998935 7.28 13 628.990 0.740 0.738 0.998784 3.43 14 657.830 0.755 0.754 0.998837 3.57 15 667.410 0.770 0.772 0.998860 3.71 16 709.816 0.786 0.785 0.999293 3.87 17 732.130 0.801 0.800 0.999300 8.02 18 755.046 0.816 0.817 0.996196 8.18	0.4337
12 602.88C 0.724 0.725 0.998935 7.28 13 628.996 0.740 0.738 0.998784 3.43 14 657.830 0.755 0.754 0.998837 3.57 15 687.410 0.770 0.772 0.998850 3.71 16 709.816 0.786 0.785 0.999293 3.87 17 732.130 0.801 0.800 0.999306 8.02 18 755.046 0.817 0.996198 8.18	0.4726
13 628.990 0.740 0.738 0.996784 1.43 14 657.830 0.755 0.754 0.996837 7.57 15 687.410 0.770 0.772 0.998860 7.71 16 709.810 0.786 0.785 0.999293 7.87 17 732.130 0.801 0.800 0.999300 8.02 18 755.046 0.817 0.996196 8.18	0.4981
14 657,830 0.755 0.754 0.998837 7.57 15 687,410 0.770 0.772 0.998860 7.71 16 709,810 0.786 0.785 0.999293 7.87 17 732,130 0.801 0.800 0.999300 8.02 18 755.046 6.516 0.817 0.996198 8.18	0.5318
15 687.410 0.770 0.772 0.998860 3.71 16 709.816 0.786 0.785 0.999293 7.87 17 732.130 0.801 0.800 0.999306 8.02 18 755.046 0.816 0.817 0.996198 8.18	9.5747
16 709.810 0.786 0.785 0.999293 7.87 17 732.130 0.801 0.800 0.999300 8.02 18 755.040 0.816 0.817 0.996198 8.18	Q. <del>(</del> 095
17 732.130 0.801 0.800 0.999306 8.02 18 755.046 0.816 0.817 0.996198 8.18	0, 6549
18 755.04G G.816 0.817 0.996196 8.18	0.7139
	0.820;
	1.6208
20 790 760 0.847 0.851 0.992997 <b>8.</b> 52	1.3776
21 801.020 0.863 0.865 0.995329 8.70	1.7914
22 808 460 Q.878 Q.878 Q.998687 \$.87	2.0693
23 815,190 0.893 0.894 0.990177 9.05	2. 2243
24 820 920 0.909 0.907 0.999075 9.25	2.3677
25 n27.730 0.924 0.924 0.998519 9.44	2.5170
26 834.34C Q.939 0.94C Q.997673 5.64	2.7611
27 #39.970 0.955 0.955 <b>0.9</b> 99681 9.86	3.0022
28 844.650 Q.970 Q.970 Q.999777 10.07	3.3895
29 848 570 0 985 0.984 0.999040 10.29	3.7945
30 852 850 1,001 1,001 0.996511 10.53	4.3312
11 #56.680 1.016 1.018 0.598283 10.77	5.0765
32 M59.210 1.031 1.030 0.99788€ 11.01.	6.0029
33 862.010 1.047 1.648 0.996877 11.28	6.6684
34 #64.070 1.062 1.063 0.99634C 11.55	6.9150
35 865,670 3,078 1.074 0.996306 11.84	7 2389
36 868.130 1.093 1.094 0.997013 12.13	7.4330
77 #70.390 3.109 1.110 0.996827 12.43	7 186 C
38 872.040 1.124 1.121 0.993903 12.76	7.4159
19 874,340 1,139 1,138 0,996783 13,09	8.3993
40 876,770 1.154 1.159 0.989513 12.43	10.6348
41 677.760 3.170 1.169 0.989847 13.81	10.7421
42 879 020 1.185 1.184 0.989141 14.19	11.3949
43 879,920 1,200 1,197 0,995324 14.58	12.6387
44 881.700 1.416	
45 882,900 1.231	
46 085.830 3.746	

10 SEPT. 1984

SPECIPEN NG.

BLC: AUTOMATIC

Page = 1050 LBF

Prin = 105 LbF F

# = C.10C

8-0.473 in. N-2.049 in

7	CYCLF	A-cor in	Amreg in	MC	deltek KSI4'n	de/de luin/cy
		••••••				
1	0.001	0.536	, ,			
;	13.500	0.551				
1 2 3 4	32.260	0.566				
ă	41.230	0.562	0.579	0.996008	7.,53	1.2302
	53.500	0.597	0.595	0.995468	7 67	1.3683
5 6	67.550	0.612	0.615	0.994753	3.02	1.5429
7	76.470	0.628	0.628	0.994854	2.90	1.0663
ė	84.350	0.643	0.643	0.993550	8.13	2.3F40
•	92.110	0.659	0.662	0.993781	8.78	2.0303
ć	95.880	0.674	0.673	0.993754	8.45	3.0144
1	99,480	0.689	0.685	0.993810	8.61	3.1873
2	105.240	0.704	0.706	0.996349	8.78	3.4732
3	109.620	0.720	0.720	0.998167	B.95	3.5348
4	114.120	0.735	0.736	0.999372	9.12	3.7205
5	117 580	0.750	0.749	0.999715	9.30	3,9463
6	121.680	0.766	0.766	0.999371	9.49	4.0449
7	125.330	0.761	0.761	0.999742	9.67	4.1358
ė	128.860	0.797	0.796	0.964399	9.87	, 4,6257
•	132.000	0.812	0.814	0.969466	10.06	6.0726
Ó	136.310	0.827	0.837	Q.971606	10.76	7.2734
i	136.750	0.843	0.840	0.970039	10.47	7 06 18
2	138.640	0.858	0.851	0.973272	10.68	7. 6290
? 3	140,990	0.873	0.875	0.979195	10.89	7.5911
4	143.020	0.889	0.889	0.996404	11.13	6. 2930
25	145.630	0.904	0.903	0.996772	11.36	5.7586
?6	148.080	0.919	0.917	0.989274	11.59	5.9411
7	151.910	0.935	0.939	0.969669	11.85	7.6493
20	154.100	0.950	9,956	0.974494	12.10	11.4294
9	155.290	0.965	0.969	0.983279	12.36	13.1061
30	155.720	0.981	0.975	0.983181	12.65	13.4561
91	156.850	0.996	0.994	0.991443	12.92	15.2028
12	158.220	1.011	1.013	0.965576	13.21	15.7095
13	159.110	1.027	1.026	0.995446	13.53	16.2237 18.9324
34	160.190	1.042	1.045	6.995221	13.84	22.2649
35	166.690	1.058	1.054	8.964507	14.19 14.53	32.8796
36	161.66	1.073	1.079	0.969686	14.88	51.6801
37	162.160	1.086	1.095	0.977532	15.27	73.6039
38	162.380	1.104	1.106	0.987862		92.8043
39	162.550	1.119	1.118	0.995951	15.65 16.05	111.4331
40	162.750	1.134	1.130	0.995944 0.990861	16.50	129.8050
4:1	162.830	1.150	1.147		16.93	183.0172
42	162.970	1.165	1.166	Q.977915 Q.954631	12.39	305.4861
43	163.080	1.100	1.169	0.953780	17.94	498,432
44	163,130	1.197 1.713	1.206	4.333180	41177	4,0,4,0
45	163.150	1.233		•		
46	163.186	1.251				

7 STPS. 1984

SPECIMEN NO.

3LC3 AUTCMATIC

Pmes - 950 LBF

Pair = 95 LBF

s . C. 106

R-0.468 in. W-2.052 in

RI	CYCLE	A-cor in	A⊣reg in	MG	deltak K51s:n	de/dn win/cy
1	0.001	0.530				
2	46 . 9 50	0.554				•
3	85.750	0.569				
4	120.780	0.584	0.587	0.992590	6.89	0.6349
5	144.630	G.600	0.602	0.996079	7.03	0.8086
6	161.740	0.615	0.616 .	0.999207	7.16	0.9411
7	173.910	0.630	C.628	0.999290	7.30	1.6511
	215.160	0.676	0.678	0.994089	7.73	3.4428
•	234.000	0.767	0.707	0.997698	B.04	3.7940
10	243,260	0.722	0.725	0.997245	8.19	2.1082
11	251.220	0.738	0.741	0.996459	8.36	2,5829
12	255,580	0.753	0.752	0.998395	8.52	2.8281
13	261,280	0.769	0.769	0.996948	8.69	3.3561
14	265.250	G.784	0.783	0.996968	8.66	3.6736
15	270,180	0.799	0.802	0.996907	9.03	3.9295
16	272.750	0.815	0.812	0.995800	9.21	4.2700
17	276.620	0.030	0.829	0.995127	9.39	4.8093
1#	280.450	0.845	0.849	0.993588	9.58	5.0141
19	282.676	0.861	0.866	0.994110	9.78	5.0005
žó	285.00C	0.876	0.873	0.995574	9,98	5.2178
21	286.710	0.891	0.892	0.994987	10.18	5.4119
22	291,720	0.907	0.908	0.997961	10.40	5.4683
23	294,48C	0.922	0.922	0.998889	10.62	5.9924
24	296.620	0.937	0.936	0.998605	10.84	6.3232
25	299.460	0.953	0.955	0.998620	11.08	6.7371
76	301.100	0.968	0.967	0.997559	11.32	6.6858
27	303,570	0.98?	0.983	0.993125	11.56	7.,0093
28	305.650	0.999	0.997	0.996667	11.84	76166
29	308.526	1.014	1.019	0.993711	12.10	8.9960
30	309.530	1.030	1.028	0.994775	12.39	9.6721
31	311.080	1.045	1.044	0.995150	12.68	11.7338
32	317.470	. 1.060	1.067	0.994878	12.97	12.5187
33	313.650	1.076	1.077	0.996219	. 13.30	13.0936
34	314.410	1.091	1.087	0.994275	13,63	14,2943
35	315.880	1.106	1,109	0.980701	13.96	18.0918
36	316.810	1.127	1.126	0.960978	14.33	279702
37	317.420	1.137	1.144	0.977254	14.70	36.9565
36	1 317,660	1.152	1.152	0.978434	15.08	40.3928
39	317.800	1.168	1.160	0.980990	15.51	42.8170
4 C	318.360	1.182	1.186	0.982153	15.93	48.0537
41	318,640 118	1.196	1.197	0.975220	16.37	56. 79 27
42	318.98	1.214	1.218	0.979087	16.86	81.9058
4.3	319, 190	1.729				
44	313.250	1.745				
45	314.360	1.260				

29 AUGUST 1984

EPECIPEN NG.

3HC 3 MANUAL

Pmex . 600 LbP

Pair = 60 LBF F = 0.100

M=0.474 in. m=2.051 in

PT I	CYCL! COUNT	A-cer in	A-1eg in	мс	deltaK RSI¢in	də/dn -uin/cy
1	0.001	0.55)			•	
Ž	90.00	0.567				
3	180.000	0.580	•	,		
4	270.000	0.589	0.590	0.997935	4.32	0.1361
5	360.00)	0.602	0.603	0.998619	4.40	0.1377
.6	450.000	0.616	0.614	0.991973	4.48	0.1579
	540.000	0.629	0.628	0.992845	4.55	0.1904
Q.	630.00)	0.641	0.645	0.995090	4.62	0.2410
• •	720.007	0.669	0.668	0.998295	4.78	0.3033
10 11	800.001	0.693	0.694	0.998624	4.93	0.3747
12	920.003	0.725 0.744	0.723	0.999031	5.13	0.4343
13	960.000	0.744	0.746	0.998627	5.75	0.4999
14	965.000	0.70	0.767 0.780	0.998224	5.40	0.5484
15	1010.000	0.797	0.795	0.998606 0.994405	5.49 5.62	0.5821 0.6797
. 16	1030.000	0.808	0.809	0.995031	5.70	0.7:96
. 17	1050.000	0.820	0.824	0.995307	5.79	0.8166
10	1070.000	0.844	0.840	0.995233	5.97	0.6843
19	1090.000	0.858	0.860	0.995339	6.08	0.9216
20	1105.000	0.876	0.875	0.996683	6.23	0.8805
21	1120.000	0.889	0.888	0.995470	6.34	0.8346
33	1135.000	0.901	0.900	0.994964	61.44	0.8318
23	1155.00C	0.913	0.915	0.996902	6.54	0.8320
24	1170.000	4.927	0.926	0.993425	6.67	0.9949
25	1185.000	0.940	0.940	0.995953	6.79	1.2460
36	1200.000	0.957	0.960	0.997581	6.96	1,5583
27 28	1215.000	0.986	0.986	0.999408	7.25	2.1353
29 29	1225.000 1230.000	1.000°	1.009	0.996323	3.49	2.7313
30	1235.000	1.027	1.023	0.997826 0.997573	7.63 3.82	2.9334 3.2323
31	1240.000	1.058	1.055	0.997388	8.67	3.2323
32	1245.000	1.071	1.074	0.997086	8.74	3.9109
33	1248.000	1.085	1.005	0,996937	8.42	4.1900
34	1251.00C	1.098	1.098	0.996262	8.60	4.2647
35	1254.00C	1.112	1.112	0.999394	. 8.8C	4.5000
36	1257.000	1.127	1.126	0.999381	9.02	4.4524
37	1260.00C	1.138	1.139	0.999420	9, 19	4.3810
30	1263.000	1.152	1.152	0.999080	9.42	4.3690
39	1266.000	1.165	1.164	0.999533	9.63	4.4048
4.0	1269.000	1.177	1.178	0.999384	9.84	4.4643
41	1272.000	1.197	1.191	0.997573	10.11	4.7143
43	1275.000 1278.000	1.206 1.218	1.205	0.996113	10.37	5.2527
44	1281.000	1.739	1.221 1.240	0.9954d3 0.998370	10.61 11.04	6. 2121
45	1282.500	1.252	1.252	0.999786	11.32	7.8759 <b>8.</b> 9448
46	1284.000	3.766	1.266	0.999989	11.64	9.9703
47	1285.500	1.282	1.281	0.991965	12.03	11.9167
48	1287.000	1.299	1.298	0.969617	12.46	14.0421
49	1289.000	1.324	1.332	0.952095	13.14	27.3839
50	1290.000	1.353	1.370	0.787949	14.02	181.5578
51	1290.500	1.369				
5.2	1291.000	1.418		•		•
53	1292.000	2.051				

19 SEPT. 1984

SPECIPER NO.

3HC? MANUAL

Pme: - 850 LBF

Prin = 85 LBF

F - 0.100

#=0.473 in. W=2.050 in

PT I	. CYCLE COUNT	ni.	A-sreg in	нс	delteR ESI <sub>4</sub> in	da/dn -uim/cy
				,		
1	0.001	0.607				
2	50.600	0.627				
3	90.000	0.647				
4	120.000	0.671	0.672	0.999061	6.81	0.8578
5	140.000	0.689	0.689	0.999390	6.97	0.9770
•	150.000	0.700	0.700	8.998059	7.06	0.9535
7	160.000	0.711	0.710	0.998721	7.16	0.9685
•	175.000	0.726	0.72,5	0.997598	730	0.9835
•	190.000	0.738	0.738	0.997610	3.41	1.0055
10	205.000	0.752	0.753	0.998533	3.54	1.0532
11	220.000	0.770	0.770	0.998480	3.71	1,1189
12	230.000	0.783	0.701	0.998952	7.84	1.1787
13	240.000	0.793	0.793	0.997702	7.94	1.7854
14	250.000	0.805	0.806	0.998387	8.06	1.3594
15	260.000	0.819	0.020	0.498634	1.21	1.4619
16	270.000	0.837	0.836	0.997859	8.41	1.5110
)7 18	277.000 284.000	0.847 0.858	0.847	0.998974	8.52	1.5177
19	291.000		0.857	0.995619	8.64	1.6025
20	298.CDO	0.867 Q.878	0.067	0.996954	8.74	1.7294
21	305.000		0.879	0.998506	8.87	2.0048
72	312.000	0.894 0.912	0.894	0.998655	9.06	2.2886
3	317.000	0.927	0.912	0.994617	9.29	2.3894
74	322.000	0.939	0.938	0.995004 0.991418	9.48	2.5826
25	327.000	0.947	0.952	0.991969	9.64 9.75	2.8151 2.9212
16	332.000	0.967	0.967	0.990767	10.02	3.0187
7	335.000	4.980	0.977	0.991358	10.21	3.1138
78	341.000	0.996	0.997	0.995864	10.45	3.3446
79	344.000	1.004	1.005	0.996815	10.58	3.1312
0 ,	347.000	1.014	1.014	0.998427	10.73	3.0556
11	350.000	1.025	1.024	0.998565	16.91	3. 221
12	353.000	1.034	1.033	0.997364	11.06	3.3451
3	359.000	1.052	1.053	0.998471	11.37	3.7529
14	365.000	1.076	1.077	0.999613	11.60	4.5434
15	368.000	1.092	1.091	0.999424	12,11	5.1572
6	371.000	1.106	1.107	0.996148	12.39	6.0091
7	374.000	3.124	1.125	0.997470	12.76	2.2763
	376.000	3.139	1.140	0.996377	13.09	9.1590
19	378.000	1.157	1.159	0.997654	13.50	11.2260
0	379.000	3.169 .	1.170	0.997924	13.79	12.3471
1	380.OCT	1.186	1.182	0.984431	14.71	16.1019
12	381.000	1.197	1.198	0.987483	14.50	20.0907
3	382.000	1.212	1.218	0.986458	14.91	28.1631
4	383.000	1.249	1.248	0.995571	16.00	42.4884
5	383.5(0	1.266	1.271	0.996559	16.55	54.9631
16	383.800	1.789	1.289	0.993358	17.35	66.1556
7	384.1(0	1.306	1.312	0.961362	17.98	113.2044
8	384.200	1.317	1.323	0.939895	18.41	184.1710
9	384.3(0	1.329				
0	384.400	1.363				

26 SEPT. 1984

SPECIMEN NG.

31:03

PANUAL

Pes - 1050 LBF

Pmin = 105 LBF

**3 - 0.100** 

B-G.468 in. W-2.051 in

PT	CYCL:F COUNT	A-ccr in	Anieg in		deltek RS1¢:n	đa/dn ulm/cy
				MC		
•	6.001	0.587				
2	20.000	0.629				
2 3	30.000	0.654				
ă	42.00C	0.696	0.692	0.998708	8.77	3.1149
Š	47.000	B.70H	0.709	0.998976	8.90	3.1608
6	57.00C	0.742	0.742	0.996490	9.29	3,5411
7	6G.000	0.751	0.751	0.998176	9.40	3.6169
. 🔅	69.000	0.78	0.786	0.998078	9.77	4.1982
	74.000	0.810	0.807	0.998440	10.13	4.7580
10	77.00C	0.821	0.622	0.997394	16.27	5.3066
11	80.000	0.836	0.838	0.996250	10.47	5.7858
12	84.000	0.860	0.861	0.999275	10.81	7.2099
13	86.000	0.877	0.876	0.999062	11.05	8.3379
14	87.000	0.883	0.884	0.998936	11.14	8.8504
35.	88.00C	0.894	0.894	0.998511	11.31	9.3623
16	89.000	0.904	0.903	0.998222	11.46	9.7143
17	90.000	0.913	0.914	0.999656	11.60	10.1060
18	91.000	0.924	0.922	0.986732	11.78	11.2024
19	92.000	0.934	0.930	0.976759	11.94	14.3421
20	93.500	0.949	0.952	0.979999	12.19	25.5182
21	34.500	0.975	0.978	0.994562	12.65	37.1320
22	95.500	1.016	1.020	0.995546	13.43	55.8495
23	96.200	1.064	1.064	6.980846	14.45	82,3913
24	96.700	1.093	1.111	0.968728	15.13	121.4061
25	97.000	1.132	1.155	0.954722	16.13	199.2155
26	97.100	1.170	1.172	0.987104	17.22	308.7769
27	97.200	1.198				5551110
28	97.250	1.231				
29	97.300	3.245				•